



# HL8941 40V, 2MHz, 0.6A Step-Down Converter

## FEATURES

- 140uA Quiescent Current
- Wide Operating Input Range 4.2V to 40V
- 600mΩ Internal Power MOSFET
- 2MHz Fixed Switching Frequency
- Internal Compensation
- High Efficiency: > 90%
- Cycle-by-Cycle Over Current Protection
- Internal Soft-Start
- 2uA Low Shutdown Supply Current
- SOT23-6L Package

## APPLICATIONS

- High Voltage Power Conversion
- Automotive Applications
- Industrial distributed power applications
- Battery Powered Equipment
- OA instrument

## PRODUCT DESCRIPTION

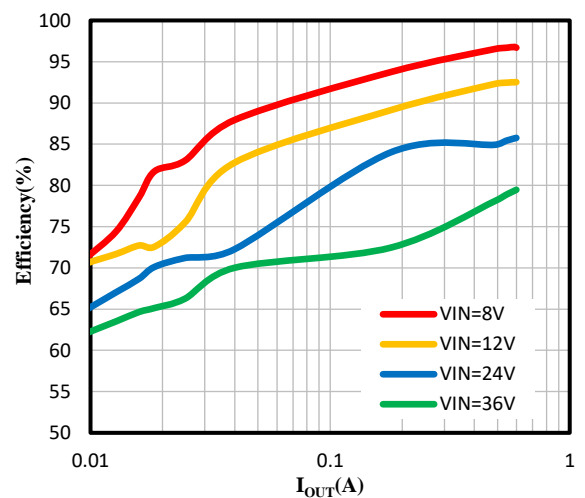
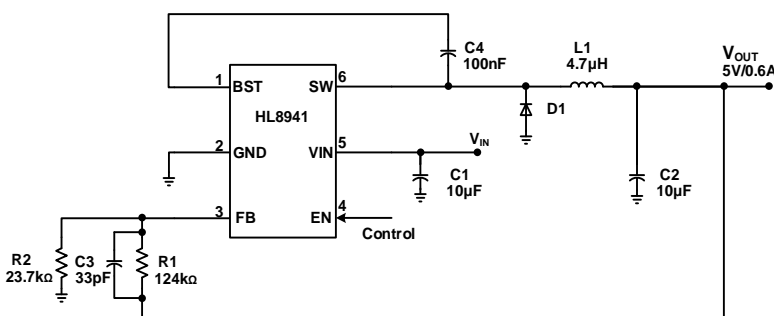
The HL8941 is a high frequency (2MHz) step-down, non-synchronous buck converter with integrated internal high-side high voltage power MOSFET. It provides 0.6A (or less) highly efficient output.

The wide 4.2V to 40V input range allows a variety of applications in automotive environment, and 2uA shutdown quiescent current allow applications in battery power systems.

Additional protection features are included such as Over Current Protection, Thermal Shutdown and Under Voltage Lockout.

The HL8941 is available in the cost-effective SOT23-6L packages.

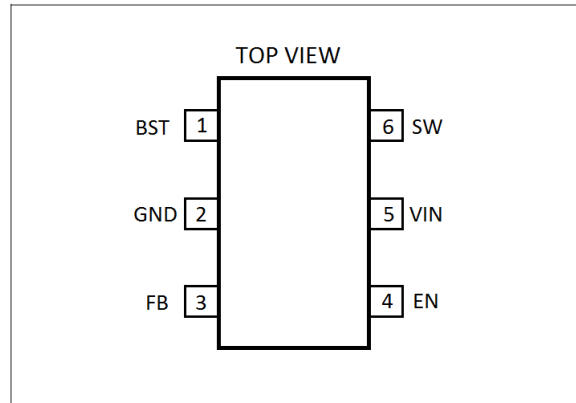
## TYPICAL APPLICATION



**ORDER INFORMATION**

MODEL	ORDER NUMBER	PACKAGE DESCRIPTION	PACKAGE OPTION	MARKING INFORMATION
HL8941	--	SOT23-6L	Tape and Reel, 3000	--

**PACKAGE REFERENCE**



**ABSOLUTE MAXIMUM RATINGS**

Supply Voltage ( $V_{IN}$ ).....	-0.3V to 40V
Switch Voltage ( $V_{SW}$ ).....	-0.3V to $V_{IN(MAX)} + 0.3V$
BST to SW.....	-0.3V to 6V
Enable ( $V_{EN}$ ) .....	40V
All Other Pins.....	-0.3V to 6V
Storage Temperature Range.....	-65°C to +150
Junction Temperature.....	150°C
Operating Temperature Range.....	-40°C to +85°C

Package Thermal Resistance @ $T_A = +25^\circ C$	
SOT23-6L, $\theta_{JA}$ .....	220°C/W
Lead Temperature (Soldering 10sec).....	260°C

NOTE:

- 1) Stresses beyond those listed “Absolute Maximum Ratings” may cause permanent damage to the device.
- 2) These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated in the operational sections of the specifications is not implied.
- 3) Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

**ESD, Electrostatic Discharge Protection**

Symbol	Parameter	Condition	Minimum Level	Unit
HBM	Human Body Model ESD		2	kV
MM	Machine Model ESD		200	V

## ELECTRICAL CHARACTERISTICS

The • denotes the specifications which apply over the full operating temperature range, otherwise specifications are At  $T_A=25^{\circ}\text{C}$ ,  $V_{IN} = 12\text{V}$ ,  $V_{EN} = 2\text{V}$ , unless otherwise noted.

PARAMETER	SYMBOL	CONDITIONS	MIN	TYP	MAX	UNITS
Feedback Voltage	$V_{FB}$	$4.0\text{V} < V_{IN} < 40\text{V}$ , $I_{OUT}=10\text{mA}$ $3.3\text{V} < V_{IN} < 4.0\text{V}$	0.778 0.770	0.794 0.794	0.810 0.818	V
Upper Switch On Resistance	$R_{DS(ON)}$	$V_{BST}-V_{SW}=5\text{V}$		600		mOhms
Upper Switch Leakage	$I_{SW\_LKG}$	$V_{EN} = 0\text{V}$ , $V_{SW} = 0\text{V}$		0.1		$\mu\text{A}$
Current Limit				1.3		A
COMP to Current Sense Transconductance	$G_{CS}$			2.7		A/V
Minimum Operating $V_{IN}$ Voltage	$V_{IN\_MIN}$		4.2			V
VIN UVLO Up Threshold	$V_{UVLO\_U}$		3.6		4.1	V
VIN UVLO Hysteresis	$V_{UVLO\_HYS}$			0.2		V
Soft-start time	$T_{SS}$	$V_{FB}$ from 0 to 0.8V		0.4		msec
Oscillator Frequency	$f_{SW}$		1600	2000	2400	kHz
Foldback Frequency	$f_{SW\_F}$			85		kHz
Minimum Switch On Time	$\tau_{ON}$			80		ns
Shutdown Supply Current	$I_{SHDN}$	$V_{EN} = 0\text{V}$		2		$\mu\text{A}$
Average Quiescent Supply Current	$I_Q$	No load, $V_{FB} = 0.9\text{V}$		140		$\mu\text{A}$
Thermal Shutdown	$T_{SD}$			155		$^{\circ}\text{C}$
Thermal Shutdown Hysteresis	$T_{SD\_HYS}$			10		$^{\circ}\text{C}$
Enable up Threshold	$V_{EN\_U}$		0.85	0.95	1.1	V
Enable Threshold Hysteresis	$V_{EN\_HYS}$			0.12		V

## PIN FUNCTIONS

Pin#	Name	Description
1	BST	SW FET Gate Bias voltage. Connect Cboot cap between BST and SW
2	GND	Ground Connection. It should be connected as close as possible to the output capacitor avoiding the high current switch paths
3	FB	Feedback Pin: Set feedback voltage divider ratio with $V_{OUT} = V_{FB} (1+(R1/R2))$
4	EN	Enable input. Pulling this pin below the specified threshold shuts the chip down. Pulling it above the specified threshold enables the chip. Floating this pin shuts the chip down
5	VIN	Input Supply.
6	SW	Switch node. This is the output from the high-side switch. A low VF Schottky diode to ground is required close to this pin to reduce switching spikes.

TYPICAL PERFORMANCE CHARACTERISTICS

$V_{IN} = 12V$ ,  $V_{OUT} = 5V$ ,  $C1 = 10\mu F$ ,  $C2 = 10\mu F$ ,  $L = 4.7\mu H$  and  $T_A = 25^\circ C$ , unless otherwise noted.

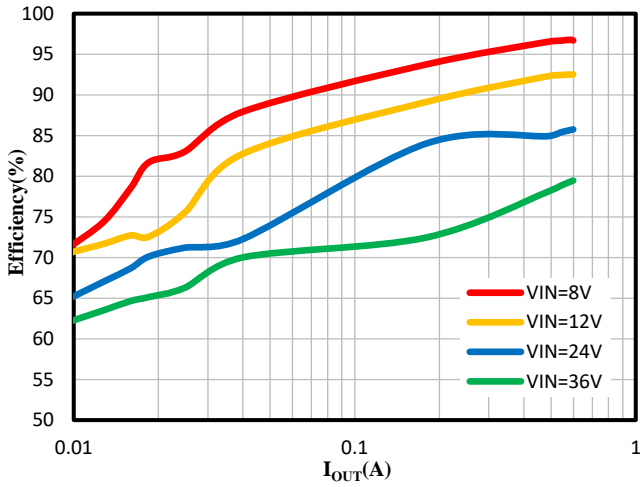


Figure 1. Efficiency,  $V_{OUT} = 5V$

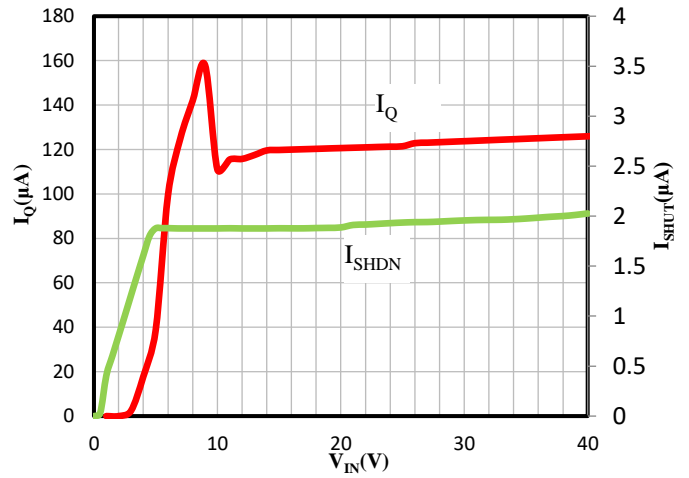


Figure 2.  $I_Q$  and  $I_{SHDN}$  vs.  $V_{IN}$

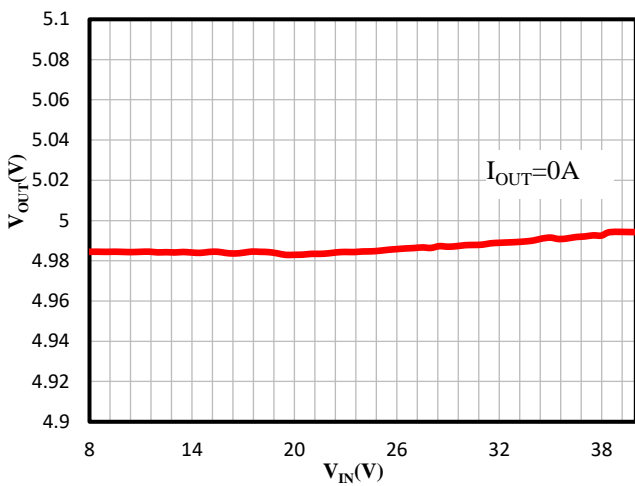


Figure 3. Line Regulation

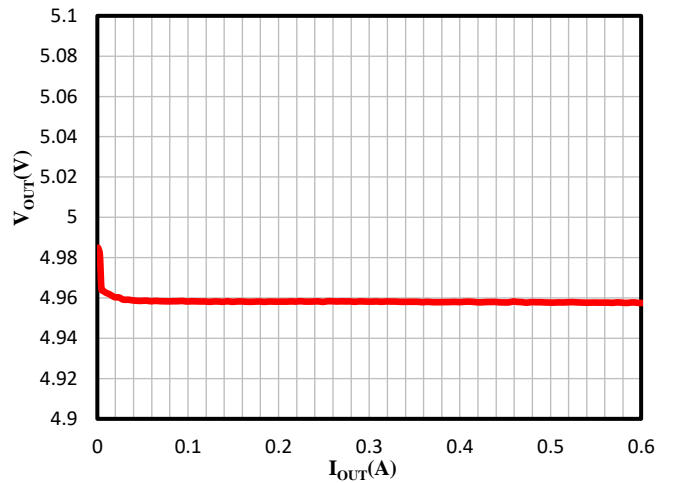


Figure 4. Load Regulation

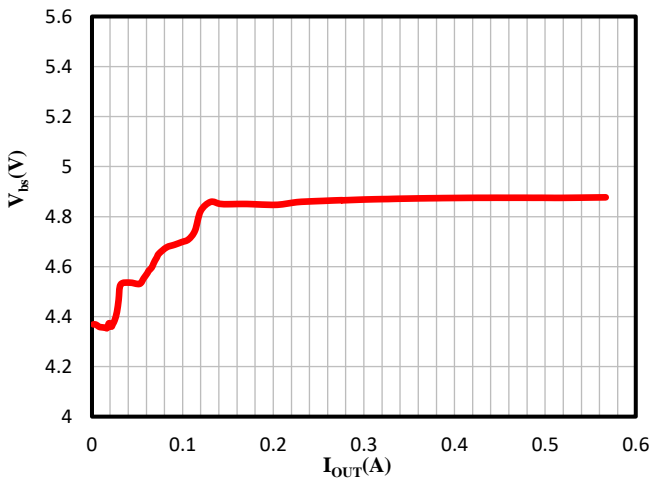


Figure 5.  $V_{BS}$  vs.  $I_{OUT}$

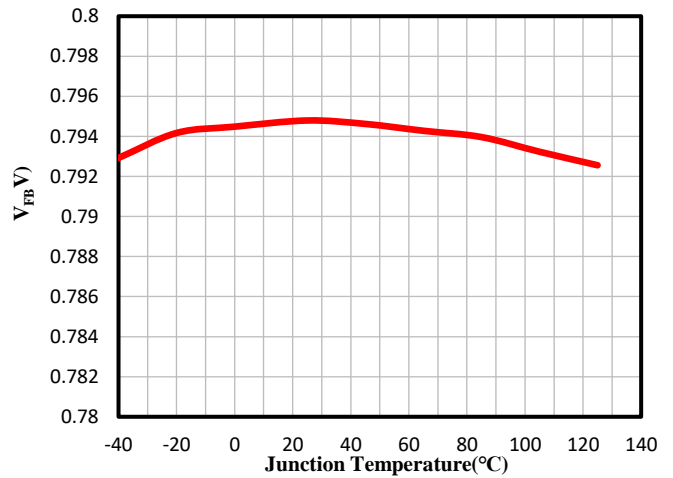


Figure 6.  $V_{FB}$  vs. Junction Temperature

TYPICAL PERFORMANCE CHARACTERISTICS

$V_{IN} = 12V$ ,  $V_{OUT} = 5V$ ,  $C1 = 10\mu F$ ,  $C2 = 10\mu F$ ,  $L = 4.7\mu H$  and  $T_A = 25^\circ C$ , unless otherwise noted.

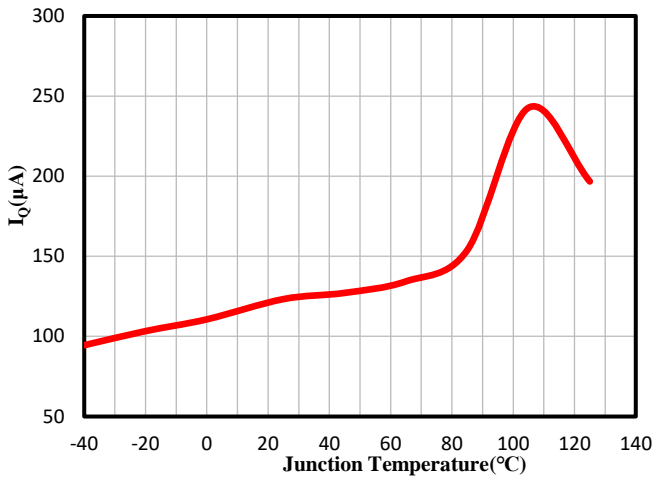


Figure 7.  $I_Q$  vs. Junction Temperature

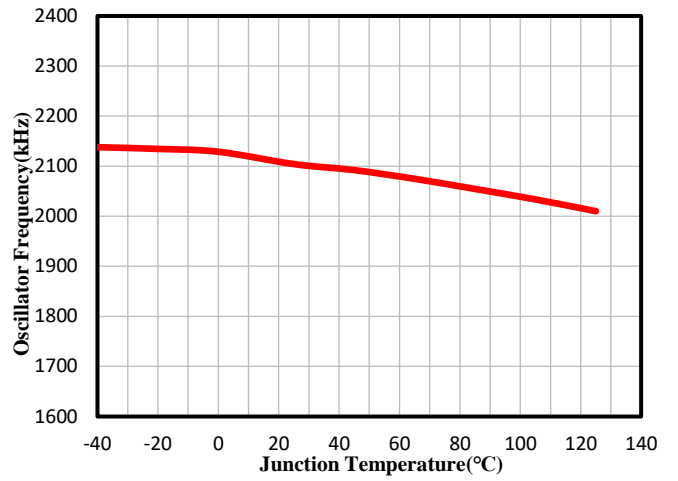


Figure 8. Oscillator Frequency vs. Junction Temperature

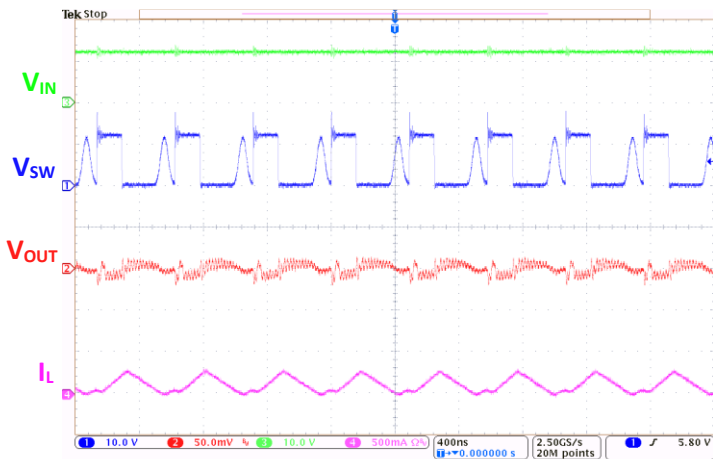


Figure 9. Steady State,  $V_{IN}=12V$ ,  $I_{OUT}=0.1A$

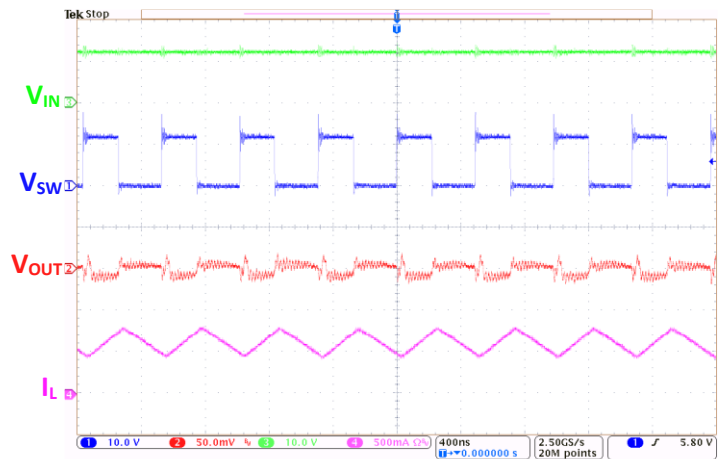


Figure 10. Steady State,  $V_{IN}=12V$ ,  $I_{OUT}=0.6A$

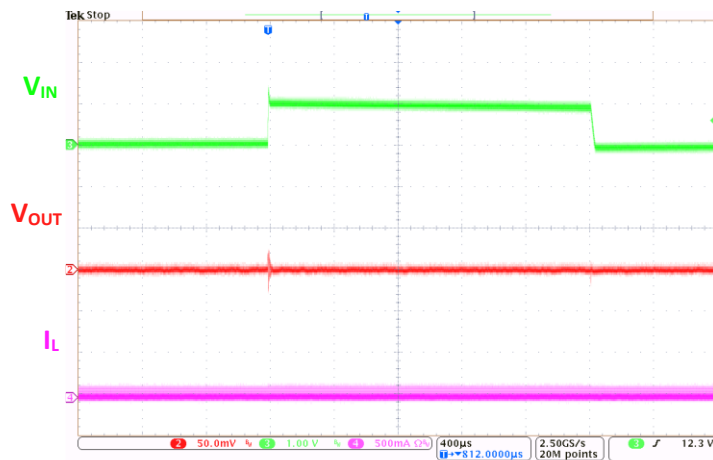


Figure 11. Line Transient  $V_{IN}=12V$  to  $13V$ ,  $I_{OUT}=0.01A$

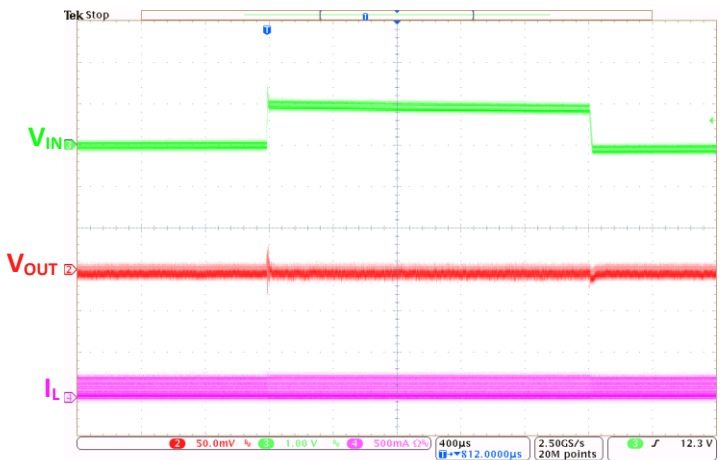


Figure 12. Line Transient  $V_{IN}=12V$  to  $13V$ ,  $I_{OUT}=0.1A$

TYPICAL PERFORMANCE CHARACTERISTICS

$V_{IN} = 12V$ ,  $V_{OUT} = 5V$ ,  $C1 = 10\mu F$ ,  $C2 = 10\mu F$ ,  $L = 4.7\mu H$  and  $T_A = 25^\circ C$ , unless otherwise noted.

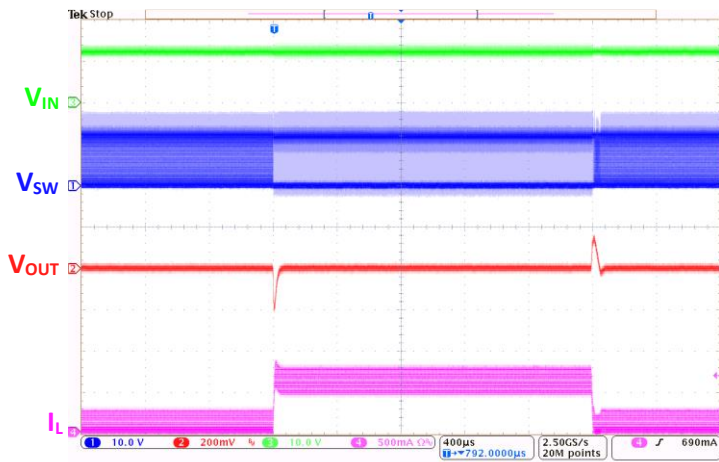


Figure 13. Load Transient,  $V_{IN}=12V$ ,  $I_{OUT}=0.1A$  to  $0.6A$

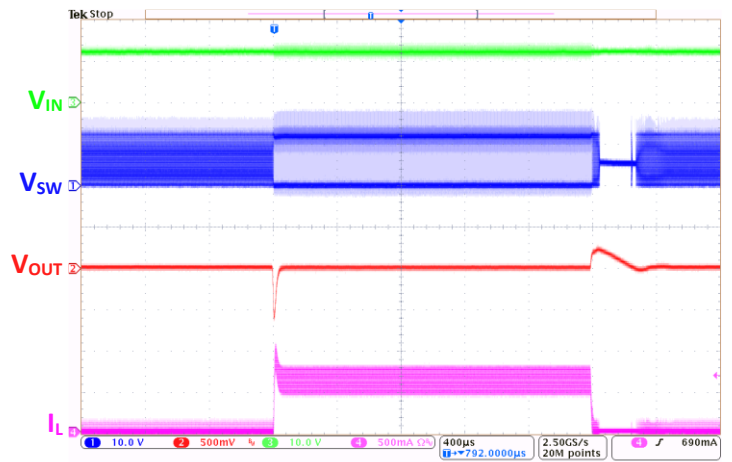


Figure 14. Load Transient,  $V_{IN}=12V$ ,  $I_{OUT}=0.01A$  to  $0.6A$

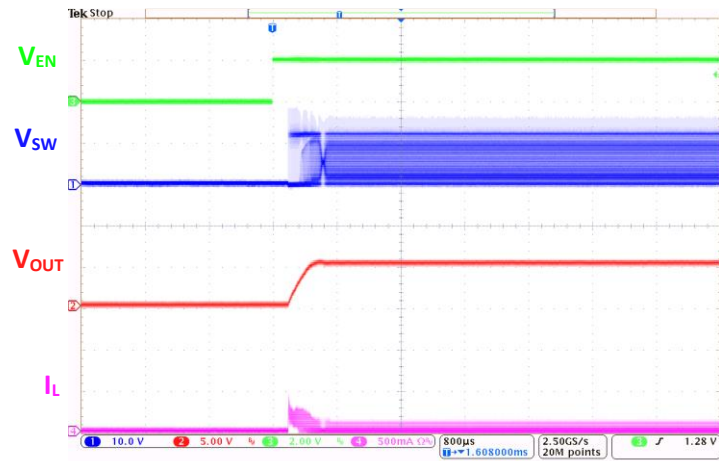


Figure 15. Startup Through EN,  $I_{OUT}=0.01A$

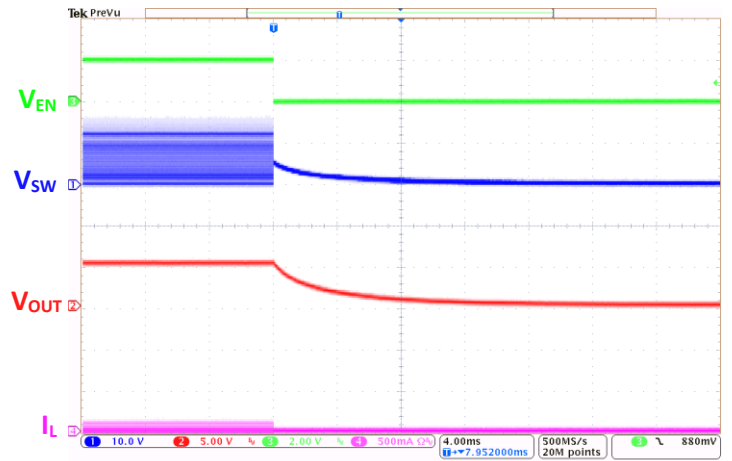


Figure 16. Shutdown Through EN,  $I_{OUT} = 0.01A$

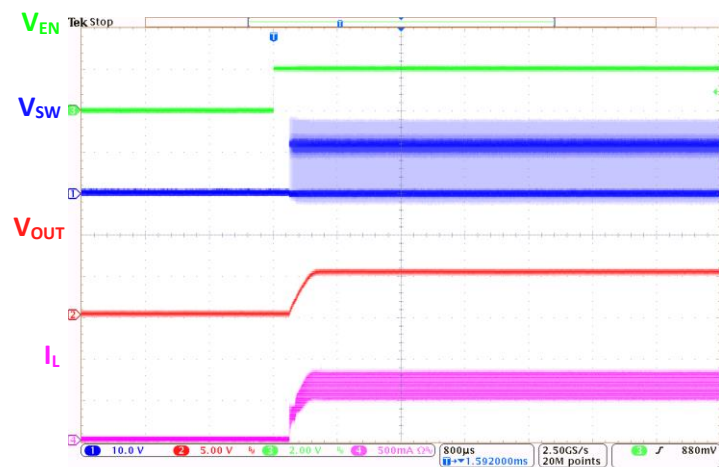


Figure 17. Startup Through EN,  $I_{OUT}=0.6A$

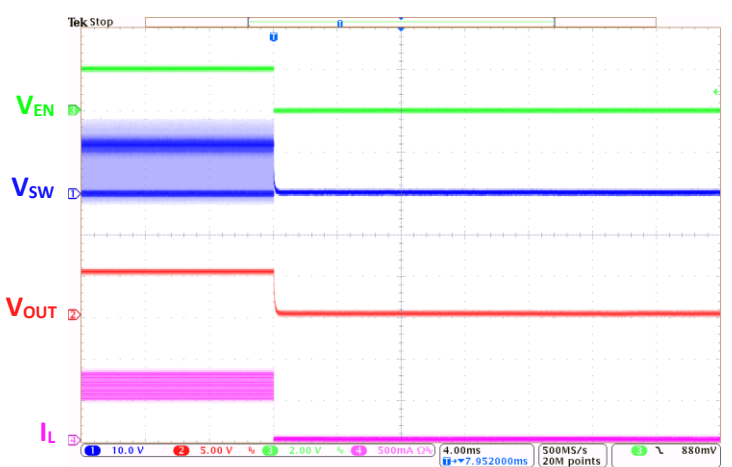


Figure 18. Shutdown Through EN,  $I_{OUT}=0.6A$

TYPICAL PERFORMANCE CHARACTERISTICS

$V_{IN} = 12V$ ,  $V_{OUT} = 5V$ ,  $C1 = 10\mu F$ ,  $C2 = 10\mu F$ ,  $L = 4.7\mu H$  and  $T_A = 25^\circ C$ , unless otherwise noted.

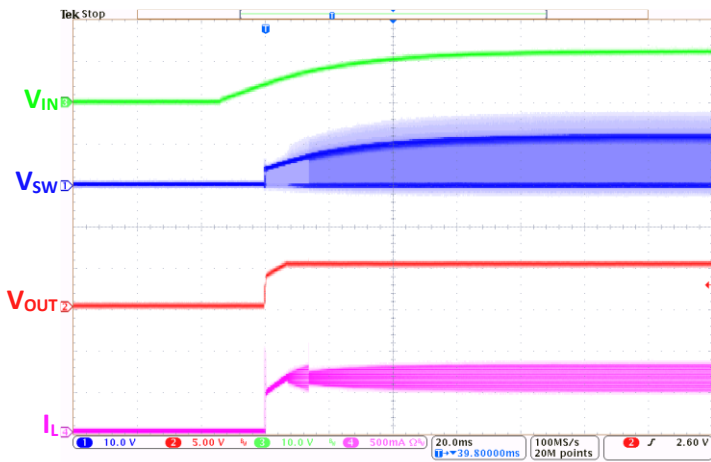


Figure 19. Power Ramp Up,  $I_{OUT} = 0.6A$

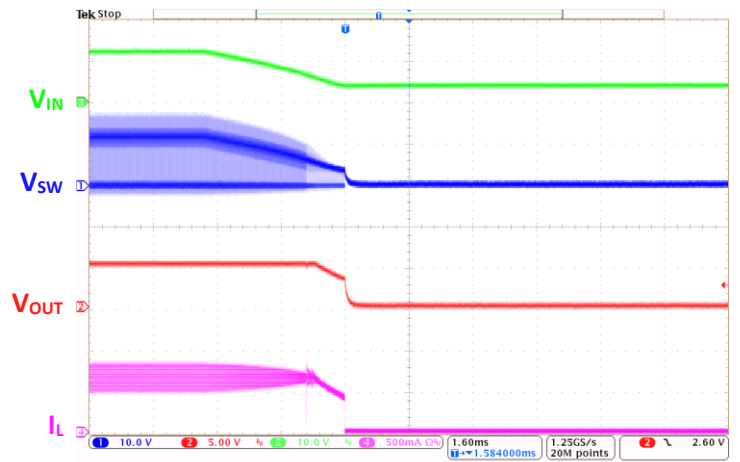


Figure 20. Power Ramp Down,  $I_{OUT} = 0.6A$

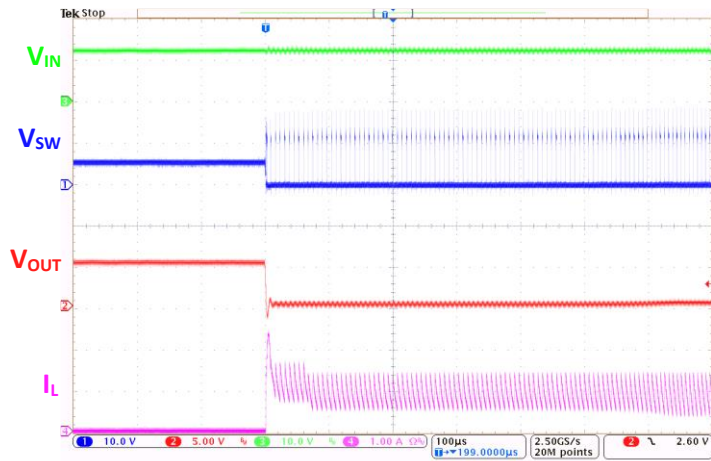


Figure 21. Short Circuit Entry,  $V_{IN} = 12V$ ,  $I_{OUT} = 0A$  to Short

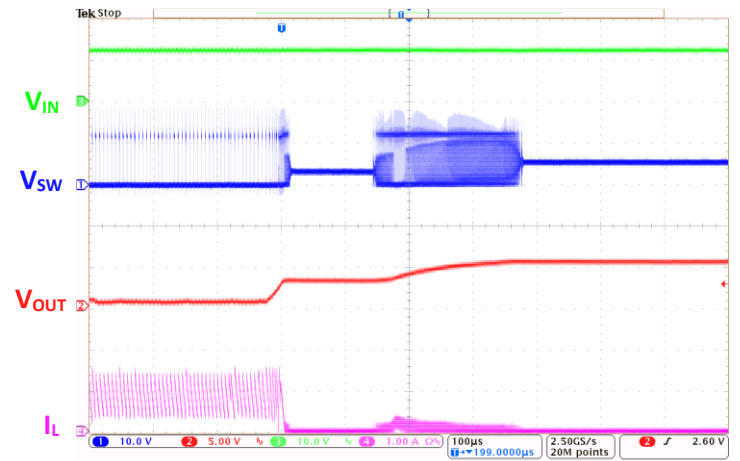


Figure 22. Short Circuit Recovery,  $V_{IN} = 12V$ ,  $I_{OUT} = \text{Short to } 0A$

FUNCTION BLOCK DIAGRAM

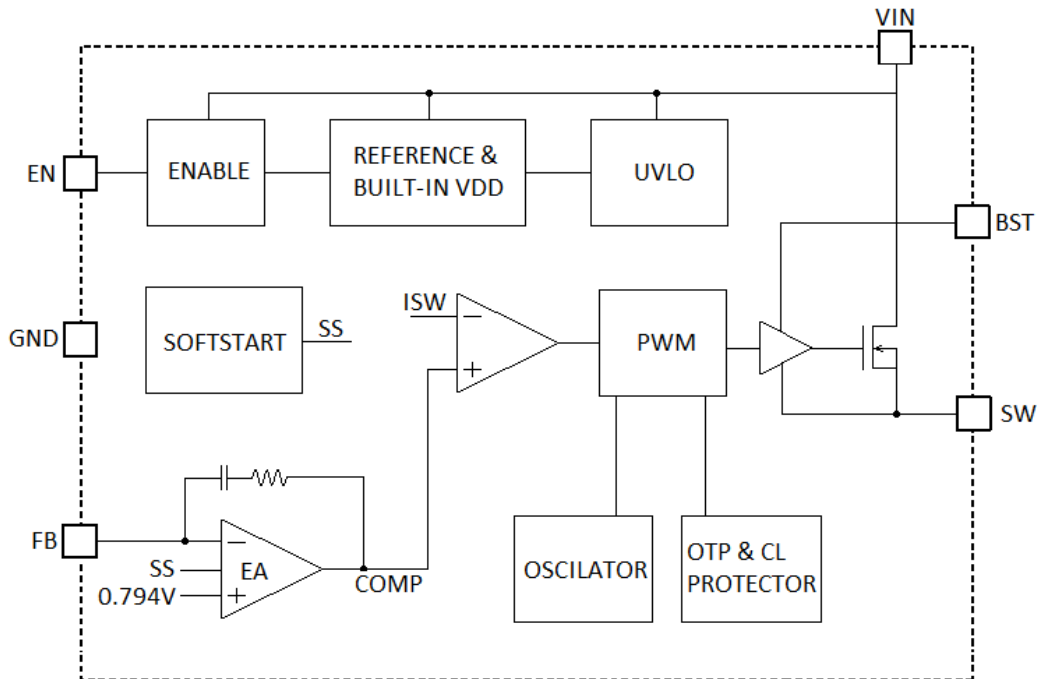


Figure 23. Function Block Diagram

OPERATION

The HL8941 is a 2MHz, non-synchronous, step-down switching regulator with integrated internal high-side high voltage power MOSFET. It provides internally compensated single 0.6A highly efficient output with current mode control. It features wide input voltage range, internal soft-start control, and precision current limit. It's very low operational quiescent current suits it for battery powered applications.

PWM Control

At moderate to high output current, the HL8941 operates in a fixed frequency, peak current control mode to regulate the output voltage. A PWM cycle is initiated by the internal clock. The power MOSFET is turned on and remains on until its current reaches the value set by COMP voltage. When the power switch is off, it remains off for at least 50ns before the next cycle

starts. If, in one PWM period, the current in the power MOSFET does not reach COMP set current value, the power MOSFET remains on until that maximum duty cycle has reached.

Pulse Skipping Mode

At light load condition, the HL8941 goes into pulse skipping mode to improve light load efficiency. Pulse skipping decision is based on its internal COMP voltage. If COMP is lower than the internal sleep threshold, a PAUSE command is generated to block the turn-on clock pulse so the power MOSFET is not commanded ON subsequently, saving gate driving and switching losses. This PAUSE command also puts the whole chip into sleep mode, consuming very low quiescent current to further improve the light load efficiency.



When COMP voltage is higher than the sleep threshold, the PAUSE signal is reset so the chip is back into normal PWM operation. Every time when the PAUSE changes states from low to high, a turn-on signal is generated right away, turning on the power MOSFET.

#### **Error Amplifier**

The Error amplifier is composed of an internal OP-AMP with an R-C feedback network connected between its output node (internal COMP node) and its negative input node (FB). When FB is lower than its internal reference voltage (REF), the COMP output is then driven higher by the OP-AMP, causing higher switch peak current output hence more energy delivered to the output. Vice versus.

When connecting to the FB pin, normally there is a voltage divider composed of  $R_{UP}$  and  $R_{DN}$  where  $R_{DN}$  is between FB and GND while  $R_{UP}$  is between the voltage output node and FB.  $R_{UP}$  serves also to control the gain of the error amplifier along with the internal compensation R- C network.

#### **Internal Regulator**

Most of the internal circuitry is powered on by the 4V internal regulator. This regulator takes  $V_{IN}$  input and operates in the full  $V_{IN}$  range. When  $V_{IN}$  is greater than 4.5V, the output of the regulator is in full regulation. When  $V_{IN}$  is lower, the output degrades.

#### **Enable Control**

The HL8941 has a dedicated enable control pin EN. With high enough  $V_{IN}$ , the chip can be enabled and disabled by EN pin. This is a HIGH effective logic. Its rising threshold is 0.93V typically and its trailing threshold is about 120mV lower. When floating, EN pin is internally pulled down to GND so the chip is disabled.

When EN is pulled down to 0V, the chip is put into the lowest shutdown current mode. When EN is higher than zero but lower than its rising threshold, the chip is still in shutdown mode but the shutdown current increases slightly.

#### **Under Voltage Lockout (UVLO)**

$V_{IN}$  Under voltage lockout (UVLO) is implemented to protect the chip from operating at insufficient supply

voltage. The UVLO rising threshold is about 4.1V while its trailing threshold is about 200mV lower.

#### **Internal Soft-start**

Reference type soft-start is implemented to prevent the converter output voltage from overshooting during startup. When the chip starts, the internal circuitry generates a soft-start voltage (SS) ramping up from 0V at a slow pace set by the soft-start time. When it is lower than the internal reference REF, SS overrides the REF so the error amplifier uses SS instead of REF as the reference. When SS is higher than REF, REF gains the control back.

SS is also associated with FB. Though SS can be much lower than FB, it can only be slightly higher than FB. If somehow FB is brought down, SS follows to track FB. This function is designed to accommodate the short-circuit recovery situation. When a short-circuit is removed, the SS ramps up as if it is a fresh soft-start process. This prevents output voltage overshoot.

#### **Thermal Shutdown**

Thermal shutdown is implemented to prevent the chip from thermally running away. When the silicon die temperature is higher than its upper threshold, it shuts down the whole chip. When the temperature is lower than its lower threshold, thermal shutdown is gone so the chip is enabled again.

#### **Floating Driver and Bootstrap Charging**

The floating power MOSFET driver is powered by an external bootstrap capacitor. This floating driver has its own UVLO protection. This UVLO's rising threshold is about 1.6V with a threshold of about 100mV. During this UVLO, the SS voltage of the controller is reset to zero. When the UVLO is removed, the controller follows soft-start process.

The bootstrap capacitor is charged to about 5V by the dedicated internal supply  $V_{CB}$ . When the voltage between SW and GND nodes is lower than its  $V_{CB}$ , a diode connected from  $V_{CB}$  to BST is turned on. The charging current path is from  $V_{IN}$ ,  $V_{CB}$ , BST and then to SW. External circuit should provide enough voltage headroom to facilitate the charging.

As long as  $V_{IN}$  is sufficiently higher than SW, the bootstrap capacitor can be charged. When the power MOSFET is ON,  $V_{IN}$  is about equal to SW so the bootstrap capacitor cannot be charged. When the external freewheeling diode is on,  $V_{IN}$  to SW difference is the largest so it is the best period to charge. When there is no current in the inductor, SW equals to the output voltage  $V_{OUT}$  so the difference between  $V_{CB}$  and  $V_{OUT}$  can be used to charge the bootstrap capacitor.

At higher duty cycle operation condition, the time period available to the bootstrap charging is less so the bootstrap capacitor may not be charged sufficiently.

In case the external circuit has not sufficient voltage and time to charge the bootstrap capacitor, extra external circuitry can be used to ensure the bootstrap voltage in normal operation region.

The floating driver's UVLO is not communicated to the controller.

#### **Current Comparator and Current Limit**

The power MOSFET current is accurately sensed via a current sense MOSFET. It is then fed to the high speed current comparator for the current mode control purpose. The current comparator takes this sensed current as one of its inputs. When the power MOSFET is turned on, the comparator is first blanked till the end of the turn-on transition to dodge the noise. Then, the comparator compares the power switch current with COMP voltage. When the sensed current is higher than COMP voltage, the comparator outputs low, turning off the power MOSFET. The maximum current of the internal power MOSFET is internally limited cycle by cycle.

#### **Startup and Shutdown**

If both  $V_{IN}$  and EN are higher than their appropriate thresholds, the chip starts. The reference block starts first, generating stable reference voltage and currents and then the internal regulator is enabled. The regulator provides stable supply for the rest circuitries.

While the internal supply rail is up, an internal timer holds the power MOSFET OFF for about 16usec to blank the startup glitches. When the internal soft-start block is enabled, it first holds its SS output low to

ensure the rest circuitries are ready and then slowly ramps up.

Three events shut down the chip: EN low,  $V_{IN}$  low, thermal shutdown. In the shutdown procedure, the signaling path is blocked first to avoid any fault triggering. COMP voltage and the internal supply rail are pulled down then. The floating driver is not subject to this shutdown command but its charging path is disabled.

**APPLICATION INFORMATION**  
**COMPONENT SELECTION**

**Setting the Output Voltage**

The output voltage is set using a resistive voltage divider from the output voltage to FB pin. The voltage divider divides the output voltage down to the feedback voltage by the ratio:

$$V_{FB} = V_{OUT} \frac{R2}{R1 + R2}$$

Thus the output voltage is:

$$V_{OUT} = V_{FB} \frac{R1 + R2}{R2}$$

The feedback resistor R1 also sets the feedback loop bandwidth with the internal compensation capacitor.

Choose R1 around 124kΩ for optimal transient response. R2 is then given by:

$$R2 = \frac{R1}{\frac{V_{OUT}}{0.8V} - 1}$$

**Table 1– Resistor Selection vs. V<sub>OUT</sub>**

V <sub>OUT</sub> (V)	R1 (kΩ)	R2 (kΩ)
0.8	124 (1%)	NS
1.2	124 (1%)	249 (1%)
3.3	124 (1%)	40.2 (1%)
5	124 (1%)	23.7 (1%)

**Inductor**

The inductor is required to supply constant current to the output load while being driven by the switched input voltage. A larger value inductor will result in less ripple current that will result in lower output ripple voltage. However, the larger value inductor will have a larger physical size, higher series resistance, and/or lower saturation current. Generally, a good rule for determining the inductance to use is to allow the peak-to-peak ripple current in the inductor to be approximately 30% of the maximum load current. Also, make sure that the peak inductor current is below the maximum switch current limit. The inductance value can be calculated by:

$$L1 = \frac{V_{OUT}}{f_s \times \Delta I_L} \times \left(1 - \frac{V_{OUT}}{V_{IN}}\right)$$

Where V<sub>OUT</sub> is the output voltage, V<sub>IN</sub> is the input voltage, f<sub>s</sub> is the switching frequency, and ΔI<sub>L</sub> is the peak-to-peak inductor ripple current.

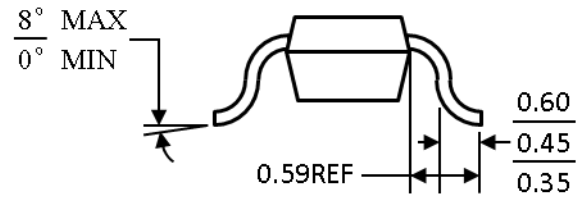
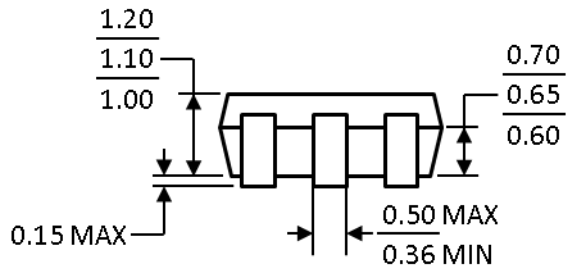
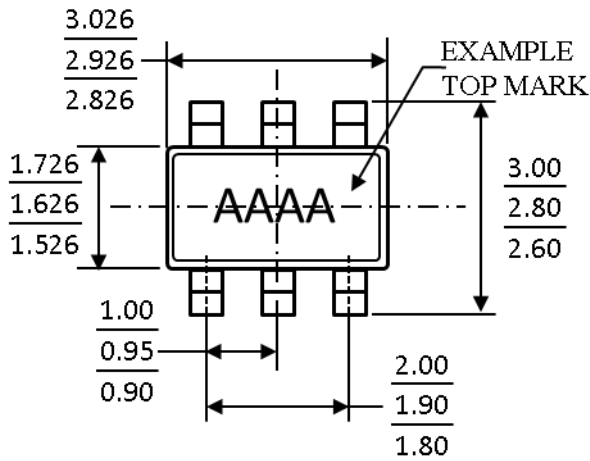
**Output Capacitor**

The output capacitor (C2) is required to maintain the DC output voltage. Ceramic, tantalum, or low ESR electrolytic capacitors are recommended. Low ESR capacitors are preferred to keep the output voltage ripple low and high efficiency.

**Table 2 — Compensation Values for Typical Output Voltage/Capacitor Combinations**

V <sub>OUT</sub> (V)	L(μH)	C2(μF)	R2(kΩ)	C3(pF)
1.2	2.2	10	249	22
2.5	2.2	10	57.6	22
3.3	2.2	10	40.2	33
5	3.3	10	23.7	33
12	6.2	10	8.87	47

PACKAGE OUTLINE DIMENSIONS



COMPLIANT TO JEDEC STANDARD MO-178-AB

Figure 24 6-Lead Small Outline Transistor Package [SOT-23]

Dimensions shown in millimeters